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# Evaluation of Hargreaves equations for estimating of reference evapotranspiration in semiarid and arid regions

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#### ABSTRACT

Penman-Monteith (FAO-56 PM) equation is suggested as the standard method for estimating evapotranspiration by the International Irrigation and Drainage Committee and FAO. On the other hand, the Hargreaves equation is an alternative method compared with the FAO-56 PM equation. In the present study, different forms of the Hargreaves equation were compared with the FAO-56 PM equation for estimating reference evapotranspiration (ET<sub>0</sub>) from 15 meteorological stations in central Iran under semi-arid and arid conditions. Also, calibrated Hargreaves (CHS) equation based on the FAO-56 PM equation was compared with new versions of this equation. The lowest and highest ratios of monthly ET<sub>0</sub> of Hargreaves equations and CHS to the FAO-56 PM reference method over all the stations were in July and December, respectively. Furthermore, a similar equation based on the mean monthly ET<sub>0</sub> calculation is derived for all selected stations. The results showed that the CHS equation gave better estimates of ET<sub>0</sub> compared to the other types of Hargreaves equations and new equation in all stations when compared to the FAO-56 PM equation as the reference equation. Also, the original Hargreaves equation was only better than the other versions of this equation in one station with high humidity and low value of wind speed during the year.

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## 1. Introduction

Water resource scarcity is a great problem attended by experts, decision makers and managers of developing countries. Due to droughts in recent years, suitable management of existing water resources and better solutions for their usage are essential (Heydari and Heydari, 2014a, 2014b).Reference evapotranspiration (ET<sub>0</sub>) of each region is generally affected by different climatic parameters as well as geographical attributes. Because a large volume of water can be lost through the soil surface, the estimation ET<sub>0</sub>has played an important role in water resource management, e.g., in irrigation engineering to define crop water requirements. (Di Stefano and Ferro, 1997; García et al. 2007; Trajkovic and Kolakovic, 2009; Marti et al., 2011; Tabari et al., 2011, 2013; Thepadia and Martinez, 2012). The measurement of the changes in ET<sub>0</sub>is very important for predicting Eco hydrological changes and natural plant communities (Monteith, 1964, 1965; Huxman et al., 2005; Mielnick et al., 2005; Prater and DeLucia, 2006). When lysimeter data of  $ET_0$  are not available, Allen et al. (1998) suggested the use of Penman-Monteith equation (FAO-56 PM) as standard method in many areas of the world. However, the major drawback of FAO-56 PM method is that air temperature; relative humidity, wind speed, and solar radiation are required which are not easily detectable in many meteorological stations.

The largest part of Iran is located in semi-arid and arid climates. On average, about 50% of all precipitation is lost by evaporation processes. Therefore, estimation of  $ET_0$  is very important (Heydari and Heydari, 2014a, 2014b; Heydari et al., 2013, 2015).

At most stations of Iran, meteorological data are often incomplete and/or not available and only maximum and minimum air temperatures are recorded, and the Hargreaves model is recommended for computation of  $ET_0$  when only air temperature data are available (Allen et al., 1998). Therefore, Hargreaves equation is an alternative method and one of the simplest equations to determinate  $ET_0$  (Hargreaves and Samani, 1985) that only requires average, maximum and minimum daily

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values of temperature and extraterrestrial radiation (Ra).

This method behaves best for weekly or longer predictions, although some accurate dailv ET<sub>0</sub>estimations have been reported in literature (Hargreaves and Allen, 2003). However, this method usually overestimates ET<sub>0</sub> at humid locations (Jensen et al., 1990, Amatya et al., 1995, Itenfisu et al., 2003, Temesgen et al., 2005; Trajkovic, 2005) and underestimates it in very dry zones, semi-arid and arid locations (Jensen et al., 1990; Allen et al., 1998; Droogers and Allen 2002; RahimiKhoob, 2008; Weiß and Menzel, 2008; Benli et al., 2010; Azhar and Perera, 2010). Moreover, the local calibration and validation of ET<sub>0</sub> models are more important in semi-arid and arid regions because most of the models have already been calibrated and validated in temperate environments (DehghaniSanij et al., 2004).

Several studies attempted to improve the accuracy of the Hargreaves equation. Chuanyan et al. (2004) tested three commonly used models to estimate monthly potential evapotranspiration (PET) values including Behnk-Maxey, Priestley-Taylor and Hargreaves in a semiarid region of China. They also provided a spatial distribution of PET and found that the Hargreaves model was the best model to estimate PET in the semiarid region of China. Martinez-Cob and Tejero-Juste (2004) showed that no local calibration would be required for windy locations (where monthly average wind speeds >2 m  $s^{-1}$  are frequent), but the C coefficient of 0.0020 instead of original 0.0023 should be used in the HS equation for non- windy locations. Vanderlinden et al. (2004) found that according to regression analysis that the C coefficient of HS equation increased to 0.0029 at coastal stations, and decreased to 0.0022 at inland stations. Both studies were made in two different semi-arid areas in Spain using data from limited number of meteorological stations, the first in the Ebro River valley, in Aragon (Northeastern Spain, 9 stations); and the second in Andalusia (southern Spain, 16 stations). Furthermore, the HS equation has been evaluated under semi-arid conditions in southern Spain from 86 meteorological stations, comparing ET<sub>0</sub> daily estimates with calculated data from the Penman Monteith equation used as standard (Gavilan et al., 2006). The results of this study showed that a regional calibration can be carried out considering only temperature and wind conditions. Trajkovic (2007) calibrated the C coefficient of HS equation using weather measurements from 10 stations in the western Balkan region (southeast Europe) and reported that in humid regions HS overestimates ET<sub>0</sub> values. Kisi (2008) compared the HS and Penman-Monteith methods in Los Angeles, USA and concluded that the calibrated HS method is the best estimating approach for evapotranspiration. Sentelhas et al. (2010) examined different reference evapotranspiration methods in Ontario, Canada and they showed by considering the amount of available weather data that the HS method can be a good

alternative to the Penman-Monteith method in Ontario, Canada. Lee (2010) found that the HS equation provides excellent results for the Korea Peninsula after local calibration as well as Jamshidi et al. (2010) and Ghamarnia et al. (2012) for different climates (dry sub-humid, moist sub-humid, semi-arid and humid) in Iran. Heydari and Heydari (2014a) calibrated C coefficient of the Hargreaves equation in these regions based on the FAO-56 PM method. The results indicated that for each stationmonth different coefficients should be used instead of the original coefficient of the Hargreaves equation (0.0023). Moreover, extensive research was required to assess the validity of different types of the Hargreaves equation for estimating  $ET_0$  in these semi-arid and arid locations. Therefore, the objective of this research was to compare the original Hargreaves equation and three new versions of this equation reported by Droogers and Allen (2002) and calibrated original Hargreaves equation (CHS) for estimating monthly ET<sub>0</sub> for 15 meteorological stations in central Iran under semi-arid and arid conditions, to complete the previous study carried out by Heydari and Heydari (2014a) in which they only considered the original Hargreaves equation.

## 2. Materials and methods

## 2.1. Site description

The study area are located in Isfahan, Ghom, Markazy, Yazd and Semnan Provinces in center of Iran (about 12% of the total area of Iran) and with almost the same latitude (N 32°-35°) and semi-arid and arid regions. Water in these areas is greatly important and over 90 % of water is used in agriculture and industry. The monthly climatic data of the 15 stations, including wind speed, the mean, maximum and minimum monthly air temperature (°C) and mean, maximum and minimum monthly air relative humidity (%) and monthly sunny hours are used with full data set from 1978 to 2007. Also, the quality of weather data such as air humidity, solar radiation, sunshine hours and wind speed was checked using the method proposed by Allen et al. (1998). Fig. 1 shows the study area (center of Iran).

Number of data (months), the mean annual temperature and mean annual rain and climate of all selected stations have been reported in Table 1.

## 2.2. PM equation

In this paper, the FAO-56 PM equation (Allen et al., 1998) is suggested as the standard method for estimating  $ET_0$ . This equation is accepted by the ASCE Task Committee on standardization of  $ET_0$ , The International Commission on Irrigation and Drainage and FAO.

The suitability of this equation has been confirmed for different climates (Ravelli and Rota, 1999; Irmak et al., 2003; Garcia et al., 2004, 2007; Zhao et al., 2005; Temesgen et al., 2005; Allen et al.,

2005, 2006; Gao et al., 2006; Jabloun and Sahli, 2008) and similar studies (Jensen et al., 1990; Allen et al., 1994a, 1994b, 1998, 2000; Smith et al., 1996; Walter et al., 2000; Gundekar et al., 2008). The FAO-

56 PM method for predicting ET<sub>0</sub> where applied on 24-h calculation time steps has the form (Allen et al., 1998):

| Table 1: Summary of weather station sites in this Stud | V |
|--|---|
|--|---|

| No.        | Weather station | Latitude<br>(N) | Longitude<br>(E) | Altitude<br>(m) | Record<br>(months) | Т<br>(°С) | V<br>(ms <sup>-1</sup> ) | RH <sub>mean</sub><br>(%) | Rain<br>(mmy-1) | Climate       |
|------------|-----------------|-----------------|------------------|-----------------|--------------------|-----------|--------------------------|---------------------------|-----------------|---------------|
| S1         | Ardestan        | 33°-23'         | 52°-23'          | 1252.40         | 168                | 18.90     | 3.6                      | 30.7                      | 115.80          | Arid          |
| S2         | Garmsar         | 35°-12'         | 52°-16'          | 825.20          | 180                | 17.40     | 2.0                      | 42.3                      | 118.70          | Arid          |
| S3         | Ghom            | 34°-42'         | 50°-51'          | 877.40          | 252                | 18.00     | 2.1                      | 41.5                      | 151.10          | Arid          |
| S4         | Golpaigan       | 33°-28'         | 50°-17'          | 1870.00         | 132                | 14.20     | 2.2                      | 38.9                      | 273.70          | Semi-<br>arid |
| S5         | Kahak           | 34°-24'         | 50°-52'          | 1403.20         | 60                 | 16.30     | 1.7                      | 39.5                      | 173.60          | Arid          |
| S6         | Kashan          | 33°-59'         | 51°-27'          | 982.30          | 348                | 19.10     | 0.6                      | 40.0                      | 138.40          | Arid          |
| S7         | Khomein         | 33°-39'         | 50°-05'          | 1835.00         | 72                 | 14.00     | 2.5                      | 39.4                      | 347.90          | Semi-<br>arid |
| <b>S</b> 8 | KhoorBiabanak   | 33°-47'         | 55°-05'          | 845.00          | 168                | 20.30     | 2.0                      | 33.8                      | 86.30           | Arid          |
| S9         | KoshkNosrat     | 35°-05'         | 50°-54'          | 948.00          | 24                 | 19.80     | 2.1                      | 41.0                      | 116.60          | Arid          |
| S10        | Meimeh          | 33°-26'         | 51°-10'          | 1980.00         | 96                 | 12.30     | 4.1                      | 37.3                      | 163.70          | Arid          |
| S11        | Naein           | 32°-51'         | 53°-05'          | 1549.00         | 168                | 16.60     | 3.1                      | 30.0                      | 98.70           | Arid          |
| S12        | Natanz          | 33°-32'         | 51°-54'          | 1684.90         | 168                | 15.50     | 2.0                      | 35.6                      | 195.30          | Arid          |
| S13        | Salafchegan     | 34°-29'         | 50°-28'          | 1380.50         | 60                 | 16.80     | 2.1                      | 42.0                      | 187.40          | Arid          |
| S14        | Saveh           | 35°-03'         | 50°-20'          | 1108.00         | 156                | 18.20     | 2.5                      | 36.4                      | 206.50          | Arid          |
| S15        | Tabas           | 33°-36'         | 56°-55'          | 976.00          | 264                | 21.70     | 1.8                      | 31.0                      | 83.20           | Arid          |

T: annual mean of air temperature; V: average wind speed; RH<sub>mean</sub>: average relative humidity; Rain: annual average precipitation; climate: with the De Martonne method



Fig. 1: Spatial distribution of the meteorological stations used in this study

$$ET_{0} = \frac{0.408 \Delta (R_{n} - G) + \gamma \left[\frac{900}{(T + 273)}\right] U_{2} (e_{s} - e_{d})}{\Delta + \gamma (1.0 + 0.34 U_{2})}$$

where  $ET_0$  = reference crop evapotranspiration (mm d<sup>-1</sup>);  $\Delta$  = slope of the saturation vapour pressure function (kPa (°C)<sup>-1</sup>); R<sub>n</sub> = net radiation (MJ m<sup>-2</sup> day<sup>-</sup> <sup>1</sup>); G = soil heat flux density (MJ m<sup>-2</sup> day<sup>-1</sup>); T = mean air temperature (°C);  $U_2$  = average 24-hour wind speed at two meters height (m s<sup>-1</sup>); e<sub>s</sub> - e<sub>d</sub> = vapour pressure deficit (kPa); and  $\gamma$  = psychometric constant (kPa (°C)<sup>-1</sup>). The factor 0.408 =  $1/\lambda$  ( $\lambda$  =

$$ET_0 = 0.0023 \times R_a \times (T_{mean} + 17.80) \times (T_{max} - 10.0023)$$

where  $ET_0$  is computed (mmd<sup>-1</sup>);  $R_a$  is the extraterrestrial radiation (mmd-1), depends on the

latent heat of vaporization in MJ kg-1) converts units from MJ  $m^{-2} d^{-1}$  to mm  $d^{-1}$ .

(1)

## 2.3. Hargreaves equations

The Hargreaves equation (Hargreaves and Samani, 1985) as original version can be written as:

$$D23 \times R_{a} \times (T_{mean} + 17.80) \times (T_{max} - T_{min})^{0.50}$$
(2)

Julian day number and latitude, and can be computed as described by Allen et al. (1998); T<sub>max</sub> and  $T_{min}$  are the daily maximum, minimum and mean air temperature (°C), 0.0023 is the original empirical coefficient proposed by Hargreaves and Samani (1985).

Droogers and Allen (2002) reported three new types of the Hargreaves equation (Hargreaves and Samani, 1985) as follows:

$$ET_{0} = 0.0030 \times R_{a} \times (T_{mean} + 20) \times (T_{max} - T_{min})^{0.40}$$
(3)

$$ET_{0} = 0.0025 \times R_{a} \times (T_{mean} + 16.80) \times (T_{max} - T_{min})^{0.50}$$
(4)

where  $ET_0$  is in mm day-1 and P is monthly rainfall (mm) and the other parameters are as presented for Equation (2).

Heydari and Heydari (2014a) calibrated C coefficient of the Hargreaves equation [Eq. 2] in these regions based on the FAO-56 PM method. The results indicated that for each station-month different coefficients should be used instead of the original coefficient of the Hargreaves equation (0.0023). The  $\text{ET}_0$  obtained in this study is referred to hereafter as CHS.

#### 2.4. Statistical analysis

For each station, statistical parameters like root mean squared error (RMSE), mean bias error (MBE) and the ratio of average  $ET_0$  estimations (R) were used to test the accuracy of  $ET_0$  determination by the following equations:

RMSE = 
$$\sqrt{\frac{\sum_{i=1}^{n} (O_i - E_i)^2}{n}}$$
 (6)

$$MBE = \frac{\sum_{i=1}^{i} (O_i - E_i)}{n}$$
(7)

$$R = \frac{O_i}{E_i} \tag{8}$$

where RMSE and MBE are in mmd<sup>-1</sup>;  $O_i$  is  $ET_0$  estimated using the Hargreaves equations (Eqs. 2-5) or CHS;  $E_i$  is  $ET_0$  estimated with the FAO-56 PM equation (Allen et al., 1998); and n is number of data (months).

#### 3. Results and discussion

Evaluation of the Hargreaves equations [Eqs. 2 to 5] and CHS equation was performed using the FAO-56 PM as reference. The average ratios between the monthly estimated  $ET_0$  with original Hargreaves equation [Eq. 2] and CHS equation to the FAO-56 PM [Eq. 1] are determined and presented in Tables 2 and 3, respectively for each station-month.

As shown in Table 2, in Ardestan, Khomein, Meimeh, Naein and Natanz regions, the average ratios between monthly estimated ET<sub>0</sub> with original Hargreaves equation to the FAO-56 PM were less than one for all months and yearly time step. Therefore, in these stations monthly  $ET_0$  estimates with the original Hargreaves equation was always less than the monthly  $ET_0$  estimates with the FAO-56 PM equation. In Kashan station, the average ratios between monthly estimated ET<sub>0</sub> with this equation to FAO-56 PM equation were more than one for all months and yearly time step. The lowest and highest values of Rwere 0.542 for Ardestan station (high wind speed combined with low humidity) in July and 1.718 for Kashan station (low wind speed combined with high humidity) in December, respectively.

The results show that the ratios between Hargreaves equation [Eq. 2] and FAO-56 PM ET<sub>0</sub> (R) ranged from 0.64 to 1.28, with a mean of 0.90 for all stations and yearly time step. After calibration and yearly time step, R ranged from 1.00 to 1.05 with an average value of 1.01 (Table 3).

Table 2: Average ratios of monthly ET<sub>0</sub> estimated using Eq. 2 and the ET<sub>0</sub> FAO-56 PM [Eq. 1]

|     | Table 2: Average ratios of monthly E10 estimated using Eq. 2 and the E10 FAO-56 PM [Eq. 1] |       |       |       |       |       |       |       |       |       |       |       |  |
|-----|--|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--|
| NO. | JAN  | FEB   | MAR   | APR   | MAY   | JUNE  | JULY  | AUG   | SEP   | OCT   | NOV   | DEC   |  |
| S1  | 0.753  | 0.681 | 0.657 | 0.636 | 0.643 | 0.607 | 0.542 | 0.552 | 0.556 | 0.573 | 0.656 | 0.816 |  |
| S2  | 1.114  | 1.018 | 0.934 | 0.909 | 0.910 | 0.873 | 0.808 | 0.842 | 1.021 | 1.061 | 1.198 | 1.368 |  |
| S3  | 1.162  | 0.998 | 0.954 | 0.964 | 0.909 | 0.865 | 0.825 | 0.892 | 1.014 | 1.070 | 1.217 | 1.357 |  |
| S4  | 1.024  | 0.832 | 0.824 | 0.818 | 0.861 | 0.884 | 0.814 | 0.894 | 0.876 | 0.884 | 0.972 | 1.081 |  |
| S5  | 1.191  | 1.021 | 0.954 | 0.968 | 0.971 | 0.991 | 0.941 | 0.968 | 1.054 | 1.051 | 1.197 | 1.323 |  |
| S6  | 1.486  | 1.235 | 1.132 | 1.119 | 1.129 | 1.183 | 1.112 | 1.121 | 1.263 | 1.325 | 1.525 | 1.718 |  |
| S7  | 0.894  | 0.881 | 0.874 | 0.862 | 0.875 | 0.924 | 0.855 | 0.890 | 0.887 | 0.857 | 0.865 | 0.925 |  |
| S8  | 1.149  | 0.983 | 0.885 | 0.855 | 0.847 | 0.839 | 0.791 | 0.863 | 0.989 | 1.080 | 1.168 | 1.425 |  |
| S9  | 1.054  | 0.905 | 0.863 | 0.860 | 0.839 | 0.810 | 0.783 | 0.832 | 0.896 | 0.918 | 1.024 | 1.199 |  |
| S10 | 0.865  | 0.796 | 0.780 | 0.811 | 0.813 | 0.804 | 0.736 | 0.793 | 0.754 | 0.778 | 0.810 | 0.892 |  |
| S11 | 0.786  | 0.729 | 0.722 | 0.742 | 0.769 | 0.747 | 0.716 | 0.732 | 0.723 | 0.722 | 0.730 | 0.836 |  |
| S12 | 0.927  | 0.801 | 0.764 | 0.779 | 0.808 | 0.784 | 0.726 | 0.744 | 0.745 | 0.753 | 0.815 | 0.966 |  |
| S13 | 1.056  | 0.915 | 0.863 | 0.879 | 0.881 | 0.884 | 0.848 | 0.881 | 0.933 | 0.911 | 1.023 | 1.154 |  |
| S14 | 0.946  | 0.812 | 0.772 | 0.756 | 0.770 | 0.756 | 0.740 | 0.773 | 0.778 | 0.766 | 0.831 | 1.043 |  |
| S15 | 1.129  | 0.977 | 0.864 | 0.819 | 0.767 | 0.744 | 0.671 | 0.699 | 0.803 | 0.871 | 0.987 | 1.132 |  |

|     | Table 5. Average ratios of monting E10 estimated using CH5 and the E10 AO-50 FM [Eq. 1] |       |       |       |       |       |       |       |       |       |       |       |
|-----|---|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| NO. | JAN   | FEB   | MAR   | APR   | MAY   | JUNE  | JULY  | AUG   | SEP   | OCT   | NOV   | DEC   |
| S1  | 1.212   | 1.095 | 1.057 | 1.024 | 1.035 | 0.996 | 0.895 | 0.910 | 0.915 | 0.921 | 1.056 | 1.313 |
| S2  | 1.163   | 1.062 | 0.974 | 0.949 | 0.950 | 0.910 | 0.843 | 0.879 | 1.066 | 1.107 | 1.250 | 1.427 |
| S3  | 1.162   | 0.998 | 0.954 | 0.964 | 0.909 | 0.865 | 0.825 | 0.892 | 1.014 | 1.070 | 1.217 | 1.357 |
| S4  | 1.157   | 0.940 | 0.937 | 0.943 | 0.973 | 0.999 | 0.935 | 1.011 | 0.990 | 0.990 | 1.099 | 1.222 |
| S5  | 1.137   | 0.979 | 0.916 | 0.936 | 0.940 | 0.958 | 0.911 | 0.938 | 1.014 | 0.999 | 1.135 | 1.250 |
| S6  | 1.163   | 0.967 | 0.886 | 0.876 | 0.884 | 0.926 | 0.871 | 0.877 | 0.988 | 1.036 | 1.193 | 1.344 |
| S7  | 1.028   | 0.985 | 0.990 | 0.988 | 1.015 | 1.085 | 0.983 | 1.025 | 1.019 | 1.002 | 0.995 | 1.086 |
| S8  | 1.199   | 1.026 | 0.924 | 0.892 | 0.883 | 0.875 | 0.826 | 0.901 | 1.033 | 1.127 | 1.218 | 1.487 |
| S9  | 1.177   | 1.011 | 0.963 | 0.958 | 0.940 | 0.909 | 0.879 | 0.933 | 0.997 | 1.018 | 1.132 | 1.336 |
| S10 | 1.090   | 1.003 | 0.984 | 1.023 | 1.025 | 1.014 | 0.958 | 1.000 | 0.968 | 0.981 | 1.021 | 1.124 |
| S11 | 1.060   | 0.982 | 0.973 | 1.000 | 1.036 | 1.007 | 0.965 | 0.987 | 0.975 | 0.973 | 0.984 | 1.126 |
| S12 | 1.169   | 1.010 | 0.963 | 0.982 | 1.019 | 0.988 | 0.916 | 0.938 | 0.940 | 0.949 | 1.055 | 1.218 |
| S13 | 1.144   | 0.993 | 0.938 | 0.957 | 0.962 | 0.965 | 0.927 | 0.962 | 1.013 | 0.981 | 1.099 | 1.243 |
| S14 | 1.193   | 1.023 | 0.973 | 0.954 | 0.971 | 0.953 | 0.933 | 0.975 | 0.981 | 0.966 | 1.048 | 1.314 |
| S15 | 1.352   | 1.174 | 1.052 | 0.997 | 0.934 | 0.906 | 0.816 | 0.852 | 0.978 | 1.060 | 1.198 | 1.378 |

 Table 3: Average ratios of monthly ET<sub>0</sub> estimated using CHS and the ET<sub>0</sub>FAO-56 PM [Eq. 1]

According to the presented results in Table 3, R values for all stations were more and less than one for cold months (December and January) and warm month (July), respectively. For stations located in semiarid regions (Khomein and Golpaigan) mean value of the R coefficient was closeto 0.90. After calibration, this value was 1.01.

The comparisons between the mean monthly  $ET_0$  values computed by the Hargreaves equations [Eqs. 2 to 5] and CHS equation against the  $ET_0$  calculated by the FAO-56 PM equation for the whole recording period of all stations are presented in Fig. 2.

As shown, the Hargreaves equations [Eqs. 2 to 5] and CHS equation performed relatively well with a  $R^2$  higher than 0.80. Table 4 and 5 shows the statistical analysis components for each station-month between  $ET_0$  estimated using the Hargreaves equations [Eqs. 2 to 5] and CHS equation and FAO-56 PM [Eq. 1]. The lowest and highest ratios monthly  $ET_0$  of Hargreaves equations and CHS to the FAO-56 PM reference method over all the stations were in July and December, respectively.

It was generally found that the Hargreaves equations [Eqs. 2 to 5] under estimates  $ET_0$  with respect to FAO-56 PM  $ET_0$  at 13 stations, and at two stations, namely Kahak and Kashan, it overestimated  $ET_0$ .

In these two stations, the monthly  $ET_0$  estimates with the Hargreaves equations [Eqs. 2 to 5] were generally higher than the monthly ET<sub>0</sub> estimates with the FAO-56 PM method. This is due to the low value of wind speed during the year in these stations, which is in agreement with previous results (Martinez-Cob and Tejero-Juste, 2004; Heydari and Heydari, 2014a). The overestimation of ET<sub>0</sub> in these stations can account for larger values of the annual average of daily temperature range  $\Delta T$  (difference between daily maximum and minimum air temperature). Also, the mean value of MBE was equal to 0.532 mm d<sup>-1</sup>, ranging from 0.091 to 1.151 mm d<sup>-1</sup>, whereas RMSE varied between 0.697 and 1.230mm d<sup>-1</sup>, with an average value of 0.862mm d<sup>-1</sup>. In the latter case, R was 1.23, indicating a mean overestimation of 23%.

The highest underestimations of the Hargreaves equations were found at Ardestan and Naein

stations: the lowest underestimations were obtained at Ghom and Garmsar stations. Moreover, the underestimations of the CHS equation were observed at all stations. As shown in Table 4 and 5, the original Hargreaves equation [Eq. 2] was only better than the other versions of this equation in Kashan region. In another 14 stations, the second version of Hargreaves equation [Eq. 3] was better than the other types of this equation except Ghom, Garmsar and Meimeh. In Ghom with arid climate the Equation (4) and in Garmsar and Meimeh with their arid climate the fourth type of Hargreaves equation [Eq. 5] which contains monthly rainfall data, was better than the other types of this equation. Considering all locations and Hargreaves equations [Eqs. 2 to 5], the maximum MBE and RMSE was in Ardestan. The minimum MBE and RMSE were in Golpaigan and Ghom, respectively. Also, the maximum and minimum R was obtained in Kashan and Ardestan, respectively.

RMSE: root mean squared error (mm d<sup>-1</sup>); MBE: mean bias error (mm d<sup>-1</sup>); R: ratio of average estimations of  $ET_0$ ; R<sup>2</sup>: coefficient of determination.

The values of RMSE, MBE and R corresponding to the comparison of  $ET_0$  FAO-56 PM and  $ET_0$ Hargreaves equation [Eq. 3] as the best equation among other Hargreaves equations for all stations ranged from 0.509 to 2.382, with a mean of 0.932 and from -2.310 to 0.897, with a mean of -0.510 and from 0.702 to 1.372, with a mean of 0.983, respectively.

Ratios of  $ET_0$  estimated using the original Hargreaves equation [Eq. 2] was closer to 1 when compared with the other versions of this equation and CHS at Ghom, Garmsar and KhoorBiabanak stations.

The Hargreaves equations [Eqs. 2 to 5] had a RMSE of less than 1.0 mm d<sup>-1</sup> only at the 7 out of 15 stations, suggesting that the model provides fairly good approximations of the FAO-56 PM method. The CHS model had a RMSE of less than 1.0 mm d<sup>-1</sup> at the all of the stations. Hence, local calibration would be required for the Hargreaves equation, especially at windy locations in the arid region.

When considering all stations in a single group, no method is clearly better than others; However, a similar equation based on mean monthly  $ET_0$  calculation with the FAO-56 PM method and other  $ET_0$  = 0.0028  $\times$  R  $_a$   $\times$  (T  $_{mean}$  +15 .44 )  $\times$  (T  $_{max}$  –

The mean value of  $ET_0$  estimates using FAO-56 PM and the new equation (Equation (9)) for 15 stations is shown in Fig. 3. Average ratios between estimates using Equation (9) and mean value  $ET_0$  estimates by FAO-56 PM are presented in Tables 5. The ratios were better compared with the Hargreaves equations [Eqs. 2 to 5].

As shown in Table 5, in Ghom, Golpaigan, Kahak, Kashan and Salafchegan stations, the average ratios

parameters used in Equation (3), was derived for all selected stations in this study as follows:

$$T_{min}$$
 )<sup>0.517</sup> (9)

between monthly estimated  $ET_0$  with Equation (9) to the FAO-56 PM were more than one, while were less than one for regions of Ardestan, Meimeh and Naein for all months and yearly time step.



Fig. 2: Comparison of ET<sub>0</sub> estimated by FAO-56 PM reference method and different Hargreaves equations for all stations. (a) Equation (2); (b) Equation (3); (c) Equation (4); (d) Equation (5)and (e) CHS

 Table 4: Comparison of statistical indices in estimating ET<sub>0</sub> values using different types of the Hargreaves equations [Eq. 2-5]

 and CHS equation and FAO-56 PM reference method [Eq. 1]

|     | and chis equation and FAO-501 M reference method [Eq. 1] |        |       |                |       |              |       |                |       |              |       |                |  |  |
|-----|--|--------|-------|----------------|-------|--------------|-------|----------------|-------|--------------|-------|----------------|--|--|
| No  | Equation (2)   |        |       |                |       | Equation (3) |       |                |       | Equation (4) |       |                |  |  |
| No. | RMSE   | MBE    | R     | R <sup>2</sup> | RMSE  | MBE          | R     | R <sup>2</sup> | RMSE  | MBE          | R     | R <sup>2</sup> |  |  |
| S1  | 2.661  | -2.603 | 0.639 | 0.889          | 2.382 | -2.308       | 0.702 | 0.893          | 2.428 | -2.367       | 0.676 | 0.890          |  |  |
| S2  | 0.814  | -0.421 | 1.005 | 0.935          | 0.780 | -0.216       | 1.074 | 0.938          | 0.707 | -0.167       | 1.058 | 0.942          |  |  |
| S3  | 0.678  | -0.324 | 1.019 | 0.959          | 0.662 | -0.147       | 1.081 | 0.962          | 0.588 | -0.063       | 1.072 | 0.965          |  |  |
| S4  | 0.661  | -0.553 | 0.897 | 0.919          | 0.509 | -0.294       | 0.978 | 0.931          | 0.515 | -0.343       | 0.942 | 0.929          |  |  |
| S5  | 0.712  | -0.091 | 1.052 | 0.945          | 0.613 | 0.116        | 1.127 | 0.949          | 0.697 | 0.155        | 1.107 | 0.946          |  |  |
| S6  | 0.774  | 0.672  | 1.279 | 0.931          | 0.969 | 0.897        | 1.373 | 0.926          | 1.002 | 0.931        | 1.348 | 0.920          |  |  |
| S7  | 0.682  | -0.621 | 0.882 | 0.945          | 0.510 | -0.401       | 0.928 | 0.958          | 0.523 | -0.403       | 0.902 | 0.953          |  |  |
| S8  | 0.839  | -0.489 | 0.990 | 0.922          | 0.716 | -0.232       | 1.061 | 0.941          | 0.774 | -0.245       | 1.045 | 0.936          |  |  |
| S9  | 1.065  | -0.772 | 0.915 | 0.925          | 0.913 | -0.519       | 0.983 | 0.934          | 0.923 | -0.529       | 0.964 | 0.933          |  |  |
| S10 | 1.062  | -1.031 | 0.803 | 0.957          | 0.899 | -0.848       | 0.861 | 0.962          | 0.862 | -0.825       | 0.842 | 0.958          |  |  |
| S11 | 1.543  | -1.454 | 0.746 | 0.944          | 1.305 | -1.211       | 0.802 | 0.953          | 1.317 | -1.220       | 0.786 | 0.951          |  |  |
| S12 | 1.051  | -0.992 | 0.801 | 0.922          | 0.788 | -0.664       | 0.898 | 0.936          | 0.880 | -0.803       | 0.842 | 0.928          |  |  |
| S13 | 0.882  | -0.561 | 0.936 | 0.935          | 0.752 | -0.346       | 1.005 | 0.953          | 0.761 | -0.327       | 0.984 | 0.948          |  |  |
| S14 | 1.453  | -1.234 | 0.812 | 0.891          | 1.244 | -0.951       | 0.885 | 0.905          | 1.258 | -0.996       | 0.855 | 0.901          |  |  |
| S15 | 1.512  | -1.282 | 0.872 | 0.905          | 1.155 | -0.913       | 0.937 | 0.921          | 1.303 | -0.998       | 0.922 | 0.917          |  |  |

| No. |       | Equation | on (5) | CHS            |       |        |       |                |  |
|-----|-------|----------|--------|----------------|-------|--------|-------|----------------|--|
| NO. | RMSE  | MBE      | R      | R <sup>2</sup> | RMSE  | MBE    | R     | R <sup>2</sup> |  |
| S1  | 2.448 | -2.400   | 0.654  | 0.889          | 0.672 | -0.212 | 1.036 | 0.919          |  |
| S2  | 0.671 | -0.119   | 1.095  | 0.959          | 0.739 | -0.234 | 1.048 | 0.942          |  |
| S3  | 0.644 | -0.108   | 1.131  | 0.963          | 0.674 | -0.324 | 1.019 | 0.959          |  |
| S4  | 0.519 | -0.321   | 0.933  | 0.930          | 0.382 | -0.072 | 1.016 | 0.942          |  |
| S5  | 0.796 | 0.429    | 1.140  | 0.939          | 0.534 | -0.185 | 1.009 | 0.961          |  |
| S6  | 1.230 | 1.151    | 1.372  | 0.895          | 0.525 | -0.269 | 1.001 | 0.951          |  |
| S7  | 0.524 | -0.194   | 0.915  | 0.954          | 0.373 | -0.051 | 1.017 | 0.973          |  |
| S8  | 0.757 | -0.287   | 1.058  | 0.936          | 0.752 | -0.303 | 1.033 | 0.954          |  |
| S9  | 0.949 | -0.332   | 0.982  | 0.932          | 0.741 | -0.273 | 1.021 | 0.936          |  |
| S10 | 0.533 | -0.452   | 0.899  | 0.971          | 0.273 | -0.024 | 1.016 | 0.978          |  |
| S11 | 1.358 | -1.257   | 0.804  | 0.945          | 0.486 | -0.064 | 1.006 | 0.961          |  |
| S12 | 1.051 | -1.000   | 0.773  | 0.922          | 0.384 | -0.132 | 1.012 | 0.953          |  |
| S13 | 0.802 | -0.127   | 1.005  | 0.940          | 0.595 | -0.161 | 1.015 | 0.951          |  |
| S14 | 1.253 | -0.993   | 0.834  | 0.900          | 0.802 | -0.212 | 1.024 | 0.912          |  |
| S15 | 1.218 | -0.916   | 0.925  | 0.915          | 0.953 | -0.291 | 1.058 | 0.924          |  |







The Equation (9) was more accurate with respect to the original Hargreaves equation and the other modified versions tested in this study, showing a reduction of nearly 10-15% in RMSE on the entire area with respect to the original Hargreaves equation. The average of RMSE for all the station months between the estimated  $ET_0$  with FAO-56 PM and Equation (9) was obtained equal to 0.840 mm d<sup>-1</sup> which was less than RMSE presented by Equation (3).

The average of RMSE was obtained 0.567 mm d-<sup>1</sup>using CHS equation. The results showed that the CHS equation gave better estimates of ET<sub>0</sub> compared to the other types of Hargreaves equations and new equation in all stations when compared to the FAO-56 PM equation as the reference equation. Using calibration and local coefficients for the most stations of this area, water consumption was reduced by 14% if the CHS equation was used instead of the original Hargreaves equation and the other modified versions. The results of this study also revealed that in arid and semiarid climates, the Hargreaves methods can be an alternative method (instead of recommended FAO-56 PM method) in estimating the regional ET<sub>0</sub>, but local calibration the coefficient of Hargreaves equation (CHS) is the best approach, where meteorological data are sparse.

|            | <b>Table 5:</b> Average ratios of monthly E1 <sub>0</sub> estimated using Eq. 9 and the E1 <sub>0</sub> FAO-56 PM [Eq. 1]. |       |       |       |       |       |       |       |       |       |       |       |  |
|------------|--|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|--|
| NO.        | JAN  | FEB   | MAR   | APR   | MAY   | JUNE  | JULY  | AUG   | SEP   | OCT   | NOV   | DEC   |  |
| S1         | 0.853  | 0.783 | 0.768 | 0.756 | 0.771 | 0.732 | 0.656 | 0.696 | 0.670 | 0.681 | 0.765 | 0.933 |  |
| S2         | 1.261  | 1.168 | 1.089 | 1.083 | 1.094 | 1.058 | 0.982 | 1.023 | 1.234 | 1.266 | 1.402 | 1.563 |  |
| S3         | 1.316  | 1.146 | 1.115 | 1.148 | 1.093 | 1.049 | 1.003 | 1.084 | 1.226 | 1.278 | 1.425 | 1.552 |  |
| S4         | 1.132  | 1.115 | 1.095 | 1.087 | 1.074 | 1.063 | 1.025 | 1.079 | 1.051 | 1.075 | 1.122 | 1.224 |  |
| S5         | 1.340  | 1.167 | 1.132 | 1.148 | 1.164 | 1.198 | 1.125 | 1.174 | 1.273 | 1.253 | 1.397 | 1.508 |  |
| S6         | 1.685  | 1.420 | 1.326 | 1.353 | 1.358 | 1.435 | 1.324 | 1.362 | 1.527 | 1.583 | 1.787 | 1.966 |  |
| S7         | 0.966  | 0.960 | 0.961 | 0.955 | 0.961 | 1.006 | 0.944 | 0.972 | 1.066 | 0.947 | 0.953 | 1.112 |  |
| <b>S</b> 8 | 1.242  | 1.141 | 1.064 | 1.035 | 1.035 | 1.026 | 0.956 | 1.035 | 1.081 | 1.279 | 1.359 | 1.633 |  |
| S9         | 1.194  | 1.038 | 1.007 | 1.022 | 1.008 | 0.981 | 0.950 | 1.010 | 1.082 | 1.096 | 1.197 | 1.372 |  |
| S10        | 0.969  | 0.935 | 0.936 | 0.952 | 0.967 | 0.968 | 0.917 | 0.957 | 0.944 | 0.921 | 0.929 | 0.978 |  |
| S11        | 0.885  | 0.891 | 0.905 | 0.886 | 0.913 | 0.902 | 0.880 | 0.886 | 0.900 | 0.892 | 0.889 | 0.925 |  |
| S12        | 1.031  | 0.905 | 0.880 | 0.915 | 0.960 | 0.940 | 0.872 | 0.894 | 0.890 | 0.887 | 0.938 | 1.089 |  |
| S13        | 1.186  | 1.044 | 1.026 | 1.041 | 1.055 | 1.068 | 1.015 | 1.068 | 1.125 | 1.086 | 1.192 | 1.314 |  |
| S14        | 1.071  | 0.930 | 0.899 | 0.896 | 0.923 | 0.913 | 0.896 | 0.936 | 0.938 | 0.913 | 0.968 | 1.191 |  |
| S15        | 1.302  | 1.138 | 1.020 | 0.981 | 0.927 | 0.904 | 0.815 | 0.850 | 0.973 | 1.047 | 1.167 | 1.314 |  |

Table 5: Average ratios of monthly ET<sub>0</sub> estimated using Eq. 9 and the ET<sub>0</sub> FAO-56 PM [Eq. 1]

4. Conclusions

In this work the FAO-56 PM model was considered as the reference standard method for

validating the predicted ET<sub>0</sub> data. Because of the lack of meteorological data for estimating monthly ET<sub>0</sub> with the FAO-56 PM method for most weather stations in the centre of Iran, original Hargreaves and different versions of this equation and calibrated Hargreaves equation (CHS) should be used for estimating monthly ET<sub>0</sub>. Application of versions of the Hargreaves equation proposed does not improve significantly or even worsen performances. The second version of Hargreaves equation [Eq. 3] was better than the other types of this equationin most of the stations. The new modified equation [Eq. 9] showed improvement in estimating ET<sub>0</sub> compared to the original and different versions of Hargreaves equation, but the CHS model presented the best performance for estimation of monthly ET<sub>0</sub> values in arid and semiarid regions (centre of Iran).Overall, calibration of the Hargreaves equation resulted in improvements of the equations by reducing the errors of the ET<sub>0</sub> estimates.

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